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RESEARCH ARTICLE

MICROSTRUCTURAL AND MECHANICAL PROPERTIES OF MODIFIED PRECIPITATION HARDENING STEEL 17-7PH AFTER MODIFICATION HEAT TREATMENT

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Abstract

Precipitation hardening stainless steel 17-7PH with modified chemical composition was heat treated by modified RH950 condition. In this paper is presented the results of tests of microstructure and mechanical properties of precipitation hardened stainless steel 17-7PH with modified chemical composition, heat treated in modified RH950 conditions. Regression analysis showed which variables are statistically significant in predicting the value of mechanical properties of the steel 17-7PH chemically modified composition.

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Introduction:-

Precipitated hardening (PH) Stainless Steels are iron-chromium-nickel alloys by the addition of one or more precipitating hardening elements such as aluminum, titanium, copper, niobium and molybdenum. Mechanical properties, such as tensile strength R_m , yield strength $R_{p0.2}$ and elongation A at elevated temperature give a lot of information about the material. Testing of the mechanical properties at elevated temperature of the samples was carried out in 16 melts, made in accordance with the design of the experiment. Regression analysis showed which variables were statistically significant for predicting value of R_m , $R_{p0.2}$ and A in steel 17-7PH with modified chemical composition.

Precipitation Hardening Stainless Steel:

Today, there are over 60 standardized and over 100 non-standardized chemical compositions stainless steel. Stainless steel is divided according to their microstructure into five groups [1,2]:

1. austenitic,
2. martensite,
3. ferrite,
4. austenitic-ferrite (duplex),
5. precipitated hardening.

Precipitation hardened stainless steels are chromium and nickel containing steels that can hold high value of strength at elevated temperatures. One of the most common grade is 17-7PH, with the composition of 17% chromium, 7% nickel and about 1% aluminum.

The advantage of this steel is their possibility to be machined in softer solution treated condition (solution annealing), and following machining or forming can be hardened by ageing heat treatment which causes low or no distortion of the component [4].

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Precipitation hardened stainless steel possess good corrosion resistance and excellent mechanical properties. Depending of the austenite stability precipitation-hardened stainless steels can be classified into classes [2,3,5,6,7]:

1. Austenitic,
2. Semi-austenitic
3. Martensitic steels.

Precipitation hardening is generally achieved from homogeneously nucleated fine precipitates of intermetallic phases [8].

Semi-austenitic PH steels:

Precipitation takes place from the indirectly obtained martensite. These steels are austenitic in the solution annealed condition. They may contain from 5 to 20% of delta ferrite [2,6,9]. Semi-austenitic steels are ductile in a solution annealed condition and are easy to machined. The content of elements that extend alpha and gamma regions must be carefully balanced to obtain the desired properties of these steels. Cooling from solution annealing temperature must be fast enough to avoid grain coarsening [2,6].

The position of PH steel in the Schaeffler-Delong diagram is given in Figure 1 [2,7,10].

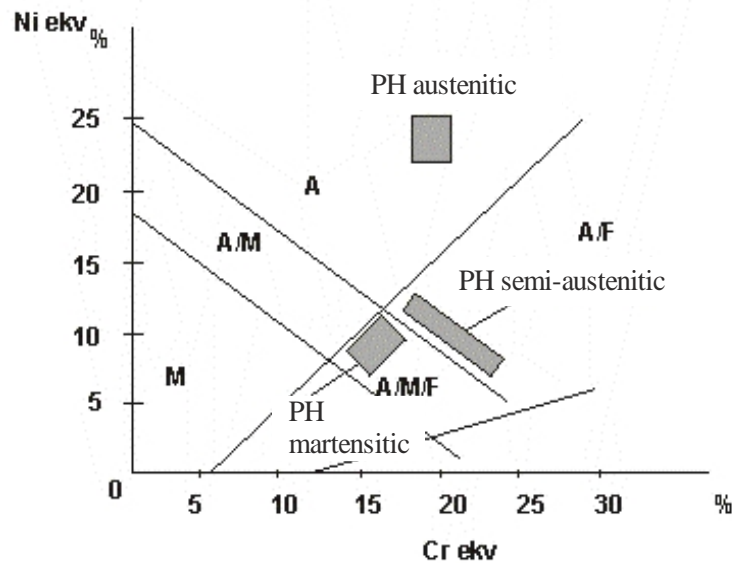


Figure 1: Location PH steels in Schaeffler-Delong diagramu [2,7].

Information Of Testing Material:

Chemical Composition:

Chemical composition of testing material and standard chemical composition for 17-7PH steel is given bellow.

Table 1:- Standard chemical composition of 17-7PH steel.

Standard	Chemical composition, [mas %]							
	C, max	Mn, Max	Si, max	P, max	S, max	Cr	Ni	Al
BAS EN 10088-5 [10]	0,09	1,0	0,7	0,040	0,015	16,0-18,0	6,5-7,8	0,7-1,5
ASTM A564/A564M [11]	0,09	1,0	1,0	0,040	0,030	16,0-18,0	6,5-7,75	0,75-1,5

Modification of chemical composition for tested batches compared with the required chemical composition of 17-7PH steel is reflected in the content of chromium, nickel and aluminum, while the content of the five basic elements (C, Si, Mn, P and S) is within the limits prescribed in Table 1, and modification of chemical composition is ranged from 13.8 to 15.7% for chromium, for nickel from 7.3 to 9.1%, while aluminum content was from 0.61 to 1.53% [2].

Making experimental samples:

For the purposes of the experiment, sixteen experimental melts were made, with an ingot weight of 6 to 8 kg. The melts were produced in semi-industrial plant, in a vacuum induction furnace. Plastic processing of forging and rolling processed at semi-industrial plants. Forging was performed on 200 t hydraulic press and air hammer B250 with several warm-ups. Forging is completed after reaching a dimension of ϕ 18 mm. Hot rolling up to a final dimension of ϕ 16 mm was carried out on a semi-industrial line SKET rolling mill, with a roller diameter of ϕ 350 mm at a temperature interval of 1150 to 950 °C [2].

Modified heat treatment RH950:

Rolled bars diameter 16 mm are heat treated solution annealing in a furnace without a protective atmosphere: heating to a temperature of 1050°C for 115 minutes, holding at 1050°C for 30 minutes and cooled in air. A diagram of the solution annealing is given in Figure 2.

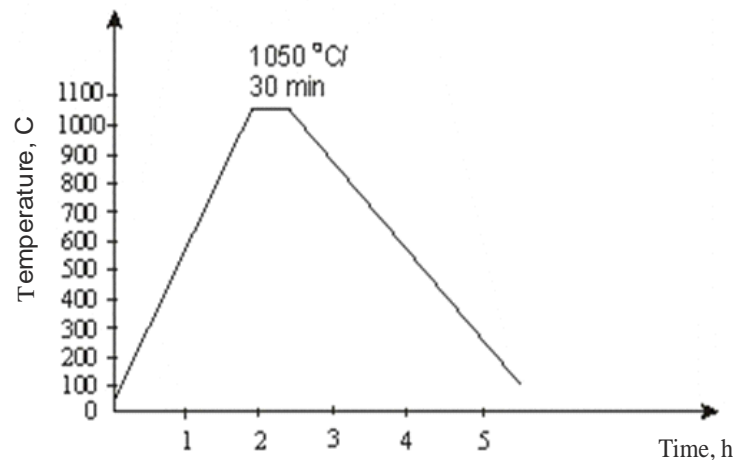


Figure 2: Diagram of solution annealing for steel with modified chemical composition 17-7PH

The high strength of precipitation hardened 17-7PH stainless steel is achieved in the following steps:

1. conditioning of austenite: heating up to 955°C for 90 minutes, holding at this temperature 10 minutes,
2. cooling below a critical temperature to transform austenite into martensite: cooling to air at room temperature, cooling to -50°C in dry ice within one hour and holding for 8 hours and heating to room temperature,
3. precipitation hardening: heating to 510°C for 45 minutes and holding at that 60 minutes and air cooling.

Diagrams of the heat treatment are given in Figure 3.

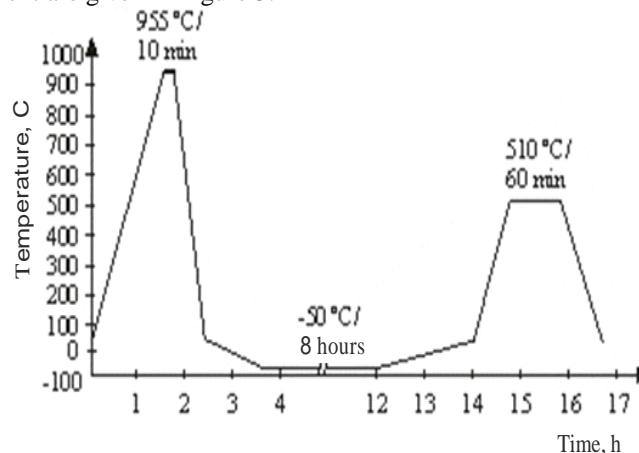


Figure 3: Diagram of precipitation annealing for steel with modified chemical composition 17-7PH

Testing Of Mechanical Properties In The Modified RH950 Condition:

The literature values of mechanical properties for 17-7PH stainless steel in condition RH950 and results of testing mechanical properties at elevated temperature for steel 17-7PH with modification chemical composition in modified RH950 condition are given in Table 2.

Table 2:- Test results of mechanical properties in modified condition RH950 at elevated temperature [2].

Literature / Batch	R _m [N/mm ²]	Rp _{0.2} [N/mm ²]	A [%]
	425 °C	425 °C	425 °C
Metals handbook [1]	-	-	-
Stainless steel [13]	1100	895	-
AK Steel bulletin [14]	1103	945	12
V1781	1030	950	11,5
V1782	1036	974	13,5
V1772	1060	968	11,5
V1773	1020	1010	12,0
V1749	959	897	8,0
V1754	1011	962	11,0
V1774	1126	1039	15,5
V1775	1082	1040	10,5
V1747	967	934	10,5
V1755	1007	962	10,0
V1760	913	891	16,5
V1783	1100	1068	12,5
V1752	1004	984	13,5
V1753	1003	921	14,5
V1750	1066	974	9,5
V1756	1056	1032	14,0

A diagrammatic overview of the results of testing mechanical properties at elevated temperature is given in Figure 4.

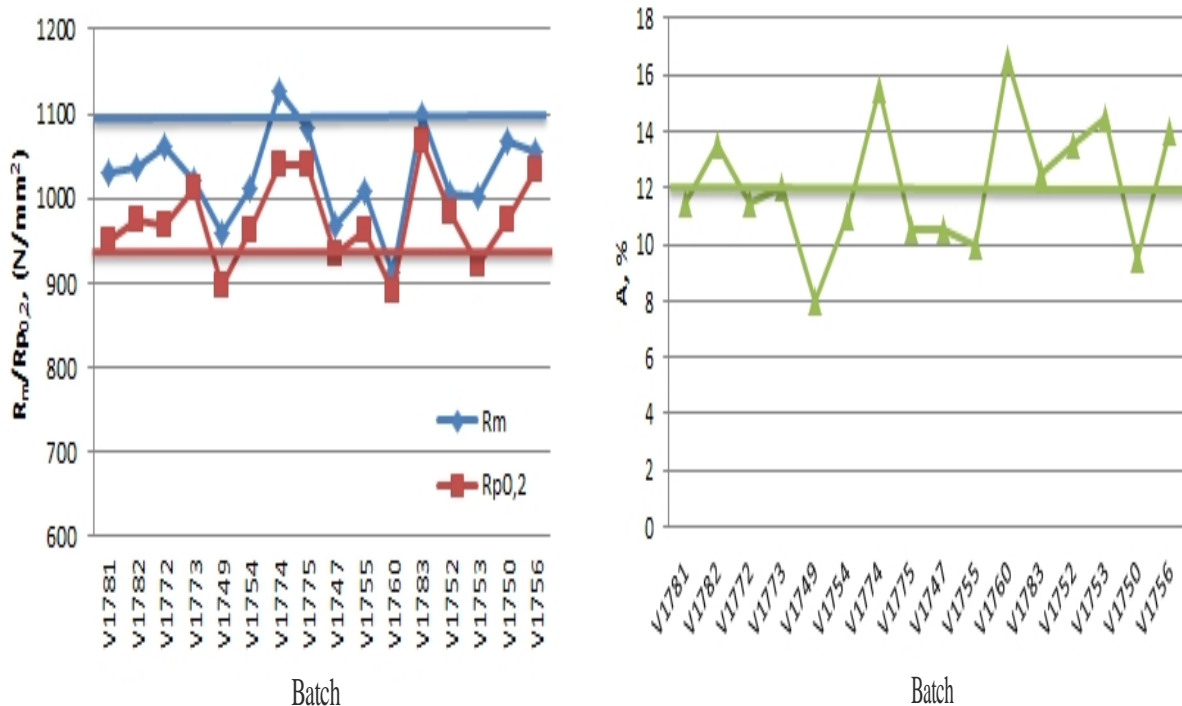


Figure 4: Diagram of results of testing mechanical properties at elevated temperature.

Mikrostructure Testing In The Modified RH950 Condition:

Metallographic analysis of samples in the modified RH950 condition revealed the microstructure of martensite and austenite and the presence of a small amount of delta ferrite. The appearance of the microstructure of specimens in the modified RH950 condition for batch V1760 and batch V1774 is given in Figures 5 and 6.

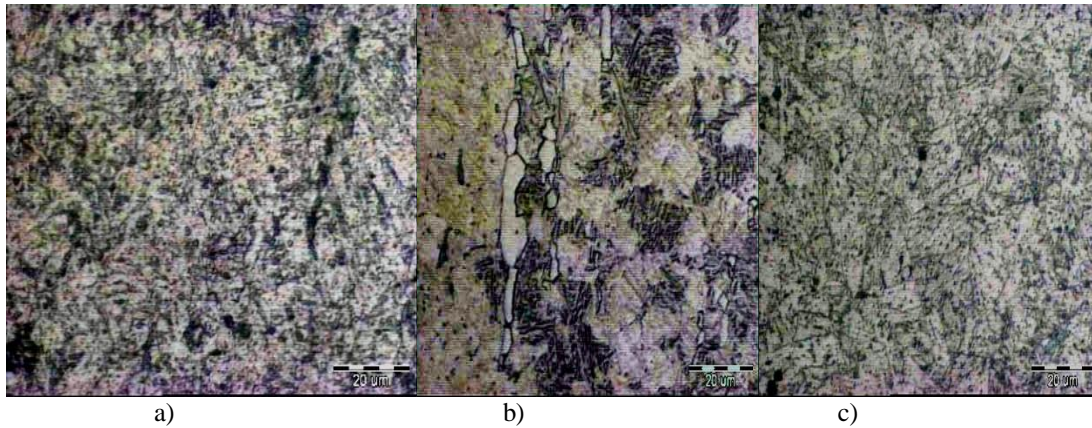


Figure 5:- Batch V1760, hardness 526HV10, a) and b) longitudinal to the rolling direction; c) transversely to the rolling direction, Kalling reagent, present 83,4% of martensite and delta ferrite and 16,6% of austenite

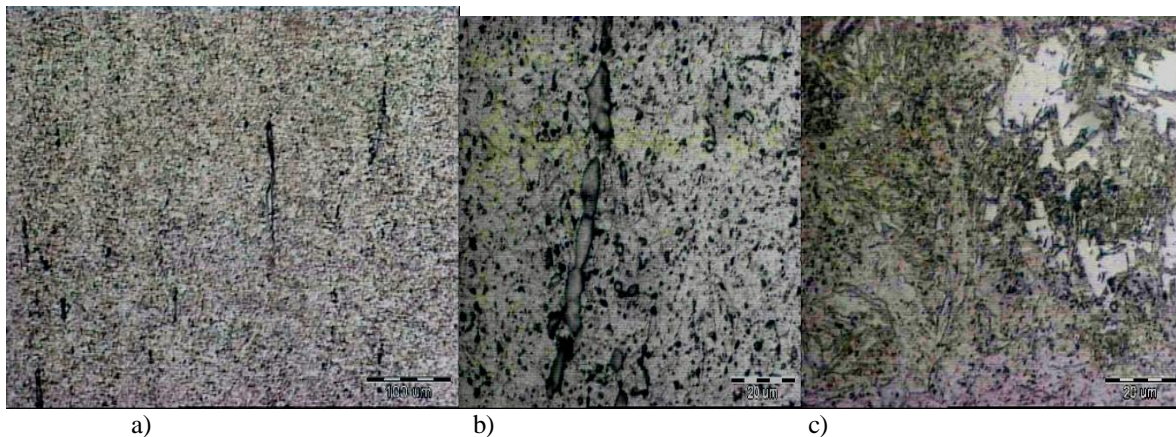


Figure 6: Batch V1774; hardness 535 HV10, a) and b) longitudinal to the rolling direction; c) transversely to the rolling direction, Kalling reagent, present 85,5% of martensite and delta ferrite and 14,5% of austenite

As microstructure show there are achieved the good percent of martensite, more than 80 percent and less than 5% of delta ferrite.

Regression Analysis Of The Effect Of Chromium, Nickel And Aluminum Content For The RH950 Condition:

Regression analysis of the results obtained by testing the mechanical properties after precipitation annealing at elevated temperature (Table 2), determined the correlation between the chromium, nickel, aluminum content and their interactions with independently variables - R_m , $R_{p0,2}$ and A.

The values of the correlation coefficients and the interrelation of independently variable chromium, nickel and aluminum, and their interactions for the modified RH950 condition are given in Table 3.

Table 3:- Correlation coefficients for the modified RH950 condition at elevated temperature.

	Cr	Ni	Al	CrNi	CrAl	NiAl	CrNiAl	$R_m/R_{p0,2}/A$
R_m	0,063	-0,344	0,396	-0,337	0,4022	0,2902	0,3023	1
Index variable	x7	x3	x2	x4	x1	x6	x5	---
$R_{p0,2}$	0,2625	-0,383	0,371	-0,267	0,4173	0,2467	0,2957	1

Index variable	x6	x2	x3	x5	x1	x7	x4	---
A	0,0817	-0,379	0,536	-0,373	0,5598	0,4080	0,4359	1
Index variable	x7	x5	x2	x6	x1	x4	x3	---

Based on the results of the regression analysis, the following regression models were selected for the modified RH950 condition:

At elevated temperature:

$$R_m = -201,68CrAl + 2624,38Al + 6,77Ni - 6,38CrNi + 20,85CrNiAl - 247,21NiAl + 108,481Cr \dots\dots\dots (1)$$

$$Rp_{0,2} = 148,94CrAl + 114,75Ni - 2073,41Al - 12,48CrNiAl - 9,82CrNi + 74,32Cr + 184,59NiAl \dots\dots\dots (2)$$

$$A = 14,52CrAl - 236,23Al - 1,71CrNiAl + 28,59NiAl + 2,89Ni - 0,55CrNi + 3,297Cr \dots\dots\dots (3)$$

The results of the regression analysis, the diagrams of the measured and predicted values, the diagrams of standardized residuals versus percentiles, and the diagrams of the standardized residuals versus regression schedules are given at figure 7 to 9.

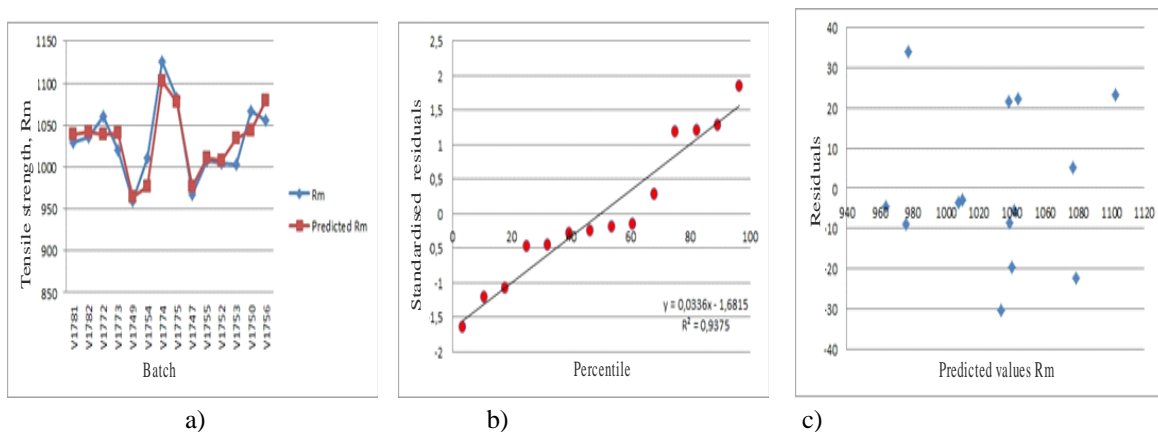


Figure 7:- Diagrams for tensile strength, R_m

a) of measured and predicted values b) of standardized residuals versus percentiles c) of residuals versus regression

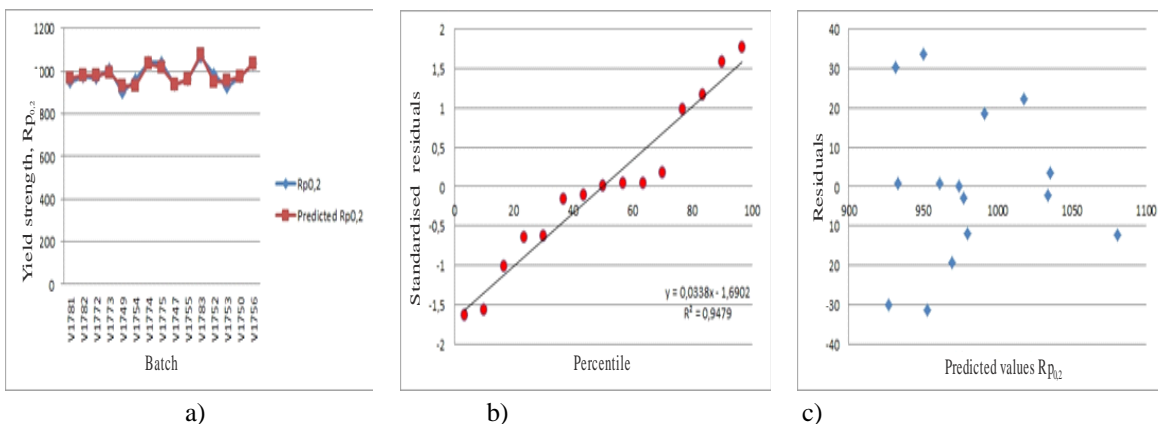


Figure 8: Diagrams for yield strength, R_{p0,2}, a) of measured and predicted values b) of standardized residuals versus percentiles c) of residuals versus regression

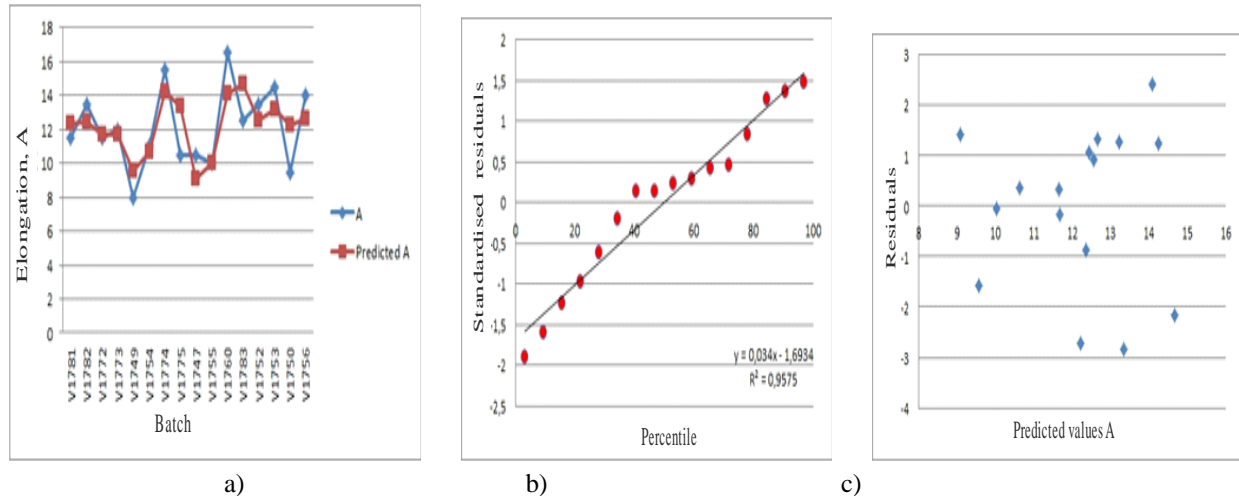


Figure 9:- Diagrams for elongation, A, a) of measured and predicted values b) of standardized residuals versus percentiles c) of residuals versus regression.

Conclusion:-

Testing of the mechanical properties at an elevated temperature of 425°C, for the modified condition RH950 showed tensile strength values in the range of 913 to 1126 N/mm², R_{p0.2} from 891 to 1068 N/mm². Elongation test results range from 8 to 16,5%. Comparing the results with the values given in the literature for the prescribed chemical composition of 17-7PH steel in the precipitated hardening condition RH950 [14], it is evident that the modified chemical composition of 17-7PH steel can achieve the values of R_m, R_{p0.2}, A and hardness HV10 above literary.

Based on the values of the coefficients in the regression models (1) to (3) in the RH950 condition at an elevated temperature of 425°C, it is observed that:

1. chromium, nickel, aluminum and the CrNiAl interaction have a positive effect, while the CrNi, CrAl and NiAl interactions have a negative effect on the tensile strength;
2. chromium, nickel and the CrAl and NiAl interactions have a positive effect, while aluminum and the CrNiAl and CrNi interactions have a negative effect on the conventional yield strength;
3. chromium, nickel and CrAl and NiAl interactions have a positive effect, while aluminum and CrNi and CrNiAl interactions have a negative effect on elongation.

Based on the Student's t-test values, it can be concluded that a statistically significant influence on the tensile strength R_m in the modified RH950 condition at the test at elevated temperature shows the Cr content, while no chemical element or a combination thereof individually shows a statistically significant influence on the values R_{p0.2} and A, but all combined, over the observed chemical composition interval, have a statistically significant influence (the value of p and F for the model in the analysis of variance).

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